Biokinectic modelling and Optimal design

British-Spanish Workshop on Optimal Design

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Compartmental analysis has applications in clinical medicine, pharmacokinetics, internal dosimetry, nuclear medicine, ecosystem studies and chemical reaction kinetics. It can be described as the analysis of a system in terms of compartments which separate the system into a finite number of component parts which are called compartments. Compartments interact through the exchange of species. Species may be a chemical substance, hormone, individuals in a population and so on.

$$\begin{vmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \end{vmatrix} = \begin{pmatrix} -(k_{10} + k_{12} + k_{13}) & k_{21} & k_{31} \\ k_{12} & -(k_{20} + k_{21} + k_{23}) & k_{32} \\ k_{13} & k_{23} & -(k_{30} + k_{31} + k_{32}) \end{vmatrix} \cdot \begin{pmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{pmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{pmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{pmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_1(t) \\ b_1(t) \\ b_2(t) \\ b_3(t) \end{bmatrix} + \begin{pmatrix} b_1(t) \\ b_1(t) \\ b_1(t) \\ b$$

Compartmental general equation

$$\mathbf{x}'(t) = \mathbf{A} \, \mathbf{x}(t) + \mathbf{b}(t)$$

$$\mathbf{x}(t) = \mathbf{x}_0 e^{t\mathbf{A}} + \int_0^t \mathbf{b}(\tau) e^{(t-\tau)\mathbf{A}} d\tau$$

 $\mathbf{x}'(t) = [x'_{1}(t), x'_{2}(t), \dots, x'_{n}(t)]^{T}$ $\mathbf{x}(t) = [x_{1}(t), x_{2}(t), \dots, x_{n}(t)]^{T}$ $\mathbf{b}(t) = [b_{1}(t), b_{2}(t), \dots, b_{n}(t)]^{T}$ $\mathbf{x0} = [x_{1}(0), x_{2}(0), \dots, x_{n}(t)]^{T}$

$$x_i(t) = \sum_{r=1}^{\infty} a_r e^{-k_r t};$$

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Catenary branches



$$r_{i}(t) = e^{-\lambda_{R}t} \sum_{C} F_{C}\left(\prod_{p=1}^{i-1} k_{p}\right) \sum_{j=1}^{i} \left(\frac{e^{-K_{j}t}}{\prod_{\substack{p=1\\p\neq j}}^{i} (K_{p} - K_{j})}\right) \quad i = 1, 2, ..., n$$

Optimal Design applied to optimization of bioassays for people exposed to intake of radioactive sustances





If a person intakes by inhalation instantaneously a quantity I, it is deposited directly in some compartments of PIS (AI, bb1, bb2, bbseq, BB1, BB2, BBseq, ET2 and ETseq) and ET1. The fraction deposited in each compartment is called Initial Deposition Factor or IDF. It is a function of Activity Median Aerodynamic Diameter (AMAD), which includes size, shape, density, anatomical and physiological parameters as well as various conditions of exposure. The . The general model of the RT is common to any element except the absorption rates {spt, sp, st} that are related with the chemical form of the element, ICRP gives default values of absorption rates according to types F, M or S.



Bioassay: Lung, urine and fecal excretion $y_i(t) = F_i(l_1, ..., l_m, s_p, s_{pt}, s_t, f_1, \lambda_1, ..., \lambda_n, h_1 ..., h_r, \lambda_R, t)$

$$r_m(t) = \sum_{j,\nu} \mathrm{IDF}_j(p) c_{j,\nu} e^{-d_{j,\nu} t_j}$$

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\begin{array}{l} -0.000186053 e^{-4.35327 \, p - 2.0001 \, t} - 0.000533918 e^{-0.170111 \, p - 2.0001 \, t} - \\ 0.0000805063 e^{-0.147244 \, p - 2.0001 \, t} + 0.0124915 e^{-0.0878945 \, p - 2.0001 \, t} + \\ 0.0213271 e^{-4.35327 \, p - 0.0301 \, t} - 0.0110729 e^{-1.11147 \, p - 0.0301 \, t} + 0.0092284 e^{-0.147244 \, p - 0.0301 \, t} + \\ 0.0110729 e^{-0.123578 \, p - 0.0301 \, t} + 0.0388835 e^{-0.170111 \, p - 0.0201 \, t} + \\ 0.0768815 e^{-0.170111 \, p - 0.0011 \, t} + 0.0106723 e^{-0.170111 \, p - 0.00022 \, t} + \\ 0.000148842 e^{-4.35327 \, p - 0.0001 \, t} - 0.00007751 e^{-1.11147 \, p - 0.0001 \, t} - \\ 0.000120097 e^{-0.566783 \, p - 0.0001 \, t} + 0.00213432 e^{-0.170111 \, p - 0.0001 \, t} + \\ 0.000064405 e^{-0.147244 \, p - 0.0001 \, t} + 0.00007751 e^{-0.123578 \, p - 0.0001 \, t} + \\ 0.0000704456 e^{-0.0878945 \, p - 0.0001 \, t} + 0.000120097 \, e^{-0.0577835 \, p - 0.0001 \, t} \end{array}
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The below method is descrited in Sánchez G; Rodríguez-Díaz J. M. 2006

Be the function $r(t, \beta)$ where, where $\beta = \{\beta_1, ..., \beta_p\}$ are parameters unknowns to be fitted using experimental data. We wish chose the best moments $\{t_0, ..., t_i, ..., t_n\}$ to take the experimental data. It will be assumed that all measured have more or less the same uncertainties, that is $\sigma^2 \simeq \sigma_i^2$. The Fisher information matrix for a specific design $\{t_1, ..., t_i, ..., t_n\} = (t_i$ is the time when the *i*-th sample should be taken) will be used the compute the optimal design. A *D*-optimal design will be a design that leads the determinant of the information matrix to a maximum.

Optdes $[R[t, \beta_1, \ldots, \beta_p], t, \{\{\beta_1, \beta_{10}\}, \ldots, \{\beta_p, \beta_{p0}\}\}, t_0, \rho, \sigma, n, opts]$ being β_1, \ldots, β_p the unknown parameters and $\beta_{10}, \ldots, \beta_{p0}$ their the initial values, t_0 is the point were is takes the first measured, ρ (relationship between samples that decays exponential), usually will be used $\rho=1$ (it is assumed that there not correlation between samples will be written "NoCorrelation"); σ is the standard deviation of the measures, n is the number of the point (additional at t_0) where we want to take measured; opts is a option to close the maximization method (The are the same that used by NMaximize). The function will give the values for $\{t_0, ..., t_i, ..., t_n\}$.

Table[{n, Optdes[inprlung[t, p], t, {{inp, 1000}, {p, 5}}, 0.5, 1, 2, n]}, {n, 1, 3}] // TableForm



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Optimal design	<u>^</u>
Home If we wish to fit the expression R[t, b1,, bp] being b1,,bp the unknown parameters to be fitted and we want take n experimental data the program gives the best moments ti where the n samples should be taken. The user must introduce as input: R[t, b1,, bp], t0 (the point were the first sample is taken); std (standard deviation of the measures) n (number of the points to take the sample, additional at t0), rho (correlation between measures, 1 by default). Help	
Compartmental Mod. A detail description of this program can be found in: G.Sanchez; J.M.Rodríguez-Díaz. Optimal design and mathematical model applied to eprograms: Radiation Protection Dosimetry.doi:10.1093/rpd/ncl499.2007. ISSN/ISBN:ISSN 1742-3406;	establish bioassay
► Doses ► Expression: a*(E^(-2.*t - 0.09*p) + E^(-0.001*t - 0.2*p)) Varia	able t t0 (point for first
► Bioassay Evaluation ► Parameters and starting points: {{a, 100}, {p, 5}} Rho (Correlation): 1 std(standard deviation): 2 Num	nber of points where to take
Statistics the samples: Evaluate	
$\underbrace{results}{(0.16647, \{t_0 \rightarrow 0.5, t_1 \rightarrow 1.98703, t_2 \rightarrow 8.16929, t_3 \rightarrow 15.0829\})}$	
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Futures Development: multiresponse models

Suppose that k_{12} and k_{23} are unknown. We want estimated k_{12} and k_{23} using experimental data of $x_2(t)$ and $x_3(t)$. The usual way is fitting $x_1 = f_1(t, k_{12}, k_{23})$ and $x_2 = f_2(t, k_{12}, k_{23})$ but the analytical expression can not be obtained.



Could be applied Optimal Design for this situation (Multiresponse problem where the analytical expression of the functions to be fitted can not be obtained however the underline SODE is known)?